

IMAGING LENS DEVICE

Related Application

[0001] This application is based on application No. 2003-198930 filed in Japan, the content of which is hereby incorporated by reference.

Field of the Invention

[0002] The present invention relates to an imaging lens device comprising an imaging sensor which converts an optical image generated on a light receiving surface of a CCD (Charge Coupled Device), a CMOS (Complementary Metal-oxide Semiconductor) sensor or the like into an electric signal, and more particularly, to an imaging lens device which serves as a principal element of a camera which is disposed within or externally attached to a digital camera, a personal computer, a mobile computer, a cellular telephone, a PDA (personal digital assistance), etc. To be more specific, the present invention relates to a compact-size imaging lens device which comprises a zoom lens system.

Description of the Prior Art

[0003] The recent years have seen an increasingly popular use of a digital camera which, using an imaging sensor such as a CCD and a CMOS sensor instead of a silver halide film, converts an optical image into an electric signal, digitizes the data and records or transfers the data. Since CCDs, CMOS sensors and the like having a high pixel count such as three or four million pixels have become recently available at relatively inexpensive prices for such digital cameras, a demand for a high-performance imaging lens device equipped with an imaging sensor is dramatically increasing,

thereby giving rise to a particularly strong demand for a compact imaging lens device which comprises a zoom lens system which is capable of zooming in and out without deteriorating an image quality.

[0004] In addition, owing to an improvement in image processing capability of a semiconductor element and the like over the recent years, imaging lens devices are more often built within or externally attached to personal computers, mobile computers, cellular telephones, PDAs (personal digital assistance) and the like these days, which further accelerates a growing demand for high-performance imaging lens devices.

[0005] Known as a zoom lens system which is favorable to be used in an imaging lens device is such a zoom lens system which comprises a first unit having a negative power, a second unit having a positive power and a third unit having a positive power disposed in this order from the object side and changes gaps between the units for zooming.

[0006] As a zoom lens system which comprises a first unit having a negative power, a second unit having a positive power and a third unit having a positive power, a zoom lens system described in Japanese Laid-Open Patent Application No. 2002-350726 for instance is known.

[0007] A zoom lens system as that according to Japanese Laid-Open Patent Application No. 2002-350726 which comprises a first unit having a negative power, a second unit having a positive power and a third unit having a positive power and changes gaps between the units for zooming has a problem that the second unit which is most dominant in realizing the zooming effect has a high eccentric sensitivity. As referred to here, an eccentric sensitivity is the magnitude of an influence over an imaging capability exerted by eccentricity which has developed between lens elements which form a zoom lens system because of a components-related error, an assembly

error, etc. In the case of an optical system having a high eccentric sensitivity, the high eccentric sensitivity increases a cost of an imaging lens device, since even the slightest eccentricity will impair an imaging capability, assembly is not easy, a high accuracy is demanded of parts and components, and more steps of adjustments and inspections become necessary during assembly. While imaging lens devices these days are becoming dramatically smaller and smaller, the smaller an imaging lens device is, the larger an influence of an eccentric sensitivity over adjustments during assembly is.

[0008] Japanese Laid-Open Patent Application No. 2002-35072 discloses to form the second unit by a positive lens and a cemented lens which is obtained by joining three lens elements of a positive lens, a negative lens and a positive lens, for the purpose of lowering the eccentric sensitivity of the second unit. However, this zoom lens system is not compact because the second unit is thick along an optical axis direction.

Summary of the Invention

[0009] In light of the problems described above, the present invention aims at providing an imaging lens device comprising a zoom lens system which has a low eccentric sensitivity but is compact and has an excellent optical capability.

[0010] To solve the problems described above, an imaging lens device according to the present invention is such an imaging lens device, comprising: a zoom lens system which comprises a plurality of lens units and changes gaps between the lens units to thereby generate an optical image of an object which can be optically and successively zoomed in and out; and an imaging sensor which converts an optical image generated by the zoom lens system into an electric signal, wherein the zoom lens system is such a zoom lens system which comprises a first unit having a negative power, a second unit having a positive power and a third unit having a positive power disposed in this order

from the object side and changes gaps between the units for zooming, there is a aperture stop disposed between the first unit and the second unit, the second unit at least one comprises one cemented lens element, which is obtained by joining three lens elements, and one lens having a positive power at least, among the three lens elements which form the cemented lens element, one lens disposed on the object side directs a convex surface toward the object side while one lens disposed on the image surface side directs a concave surface toward the image surface side, and the following condition expressions are satisfied:

$$-0.2 < (R21 - R24) / (R21 + R24) < 1.0$$

$$0.6 < R21 / Fw < 10.0$$

$$0.0 \leq h2 / ha4 < 1.0$$

where

R21 : a paraxial radius of curvature of the object side-lens surface of the cemented lens element,

R24 : a paraxial radius of curvature of the image surface side-lens surface of the cemented lens element,

Fw : a focal length of the overall system at the wide-angle end,

ha4 : a distance from an optical axis of an intersection of a principal ray which is at 0.8X of a maximum half-angle of view ω at the wide-angle end and the image surface side-lens surface of the cemented lens element,

h2 : a distance from an optical axis of an intersection of a principal ray which is at 0.8X of a maximum half-angle of view ω at the wide-angle end and the outermost lens surface of the second unit toward the object side,

and where a principal ray is a ray which propagates on the center of the aperture stop.

[0011] In a different aspect, the present invention is characterized in being directed

to a digital camera which comprises the imaging lens device described above.

Although the term "digital camera" used to exclusively refer to those which record still optical images, those digital cameras are not particularly distinguished these days from digital cameras which can also handle moving images, household digital video cameras and the like which have been proposed. Hence, as herein referred to, digital cameras include all cameras whose principal element is an imaging lens device comprising an imaging sensor of a digital still camera, a digital movie camera and the like which converts an optical image generated on a light receiving surface of the imaging sensor into an electric signal.

Brief Description of the Drawings

[0012] This and other objects and features of this invention will become clear from the following description, taken in conjunction with the preferred embodiments with reference to the accompanied drawings in which:

- Fig. 1 is a lens construction view of a first embodiment (first example);
- Fig. 2 is a lens construction view of a second embodiment (second example);
- Fig. 3 is a lens construction view of a third embodiment (third example);
- Fig. 4 is a lens construction view of a fourth embodiment (fourth example);
- Fig. 5 is a lens construction view of a fifth embodiment (fifth example);
- Fig. 6 is a lens construction view of a sixth embodiment (sixth example);
- Fig. 7 is a lens construction view of a seventh embodiment (seventh example);
- Fig. 8 is a lens construction view of an eighth embodiment (eighth example);
- Fig. 9 is a lens construction view of a ninth embodiment (ninth example);
- Fig. 10 is a lens construction view of a tenth embodiment (tenth example);
- Fig. 11 is graphic representations of aberrations of the first embodiment in

in-focus state at infinity;

Fig. 12 is graphic representations of aberrations of the second embodiment in in-focus state at infinity;

Fig. 13 is graphic representations of aberrations of the third embodiment in in-focus state at infinity;

Fig. 14 is graphic representations of aberrations of the fourth embodiment in in-focus state at infinity;

Fig. 15 is graphic representations of aberrations of the fifth embodiment in in-focus state at infinity;

Fig. 16 is graphic representations of aberrations of the sixth embodiment in in-focus state at infinity;

Fig. 17 is graphic representations of aberrations of the seventh embodiment in in-focus state at infinity;

Fig. 18 is graphic representations of aberrations of the eighth embodiment in in-focus state at infinity;

Fig. 19 is graphic representations of aberrations of the ninth embodiment in in-focus state at infinity;

Fig. 20 is graphic representations of aberrations of the tenth embodiment in in-focus state at infinity; and

Fig. 21 is a construction view showing the present invention in outline.

Description of the Preferred Embodiments

[0013] Preferred embodiments of the present invention will now be described with reference to associated drawings. An imaging lens device which is one preferred embodiment of the present invention, as shown in Fig. 21 for instance, comprises a

zoom lens system TL which generates an optical image of an object which can be zoomed in and out, an optical low pass filter LPF, and an imaging sensor SR which converts an optical image generated by the zoom lens system TL into an electric signal, all of which are disposed in this order from the object side. Further, the zoom lens system comprises a first lens unit Gr1 including a prism PR which internally comprises a reflection surface, and subsequent lens units. The imaging lens device is a principal element of a camera which is disposed within or externally attached to a digital camera, a video camera, a personal computer, a mobile computer, a cellular telephone, a PDA (personal digital assistance), etc.

[0014] The zoom lens system TL comprises a plurality of lens units including the first lens units Gr1, and is capable of changing the size of an optical image by changing gaps between the lens units. The first lens unit Gr1 has a negative power, and may internally comprise a prism PR which bends an optical axis of an object ray by about 90 degrees, in which case the apparent thickness can be reduced.

[0015] The optical low pass filter LPF has a particular cutoff frequency for adjusting a spatial frequency characteristic of the imaging lens system and eliminating a color moiré which is created in the imaging sensor. The optical low pass filter according to the preferred embodiment is a birefringent low pass filter which is obtained by stacking a birefringent material such as crystals whose crystal axes are aligned in a predetermined direction, a wavelength plate which changes a plane of polarization, and the like one atop the other. The optical low pass filter may be a phase-type low pass filter or the like which realizes a required optical characteristic related to a cutoff frequency by means of diffraction. The optical low pass filter is not essentially required. It is possible to omit the optical low pass filter by executing the other image processing method, such as electrically image processing method.

[0016] The imaging sensor SR comprises a CCD having a plurality of pixels and converts an optical image generated by the zoom lens system into an electric signal using the CCD. The signal generated by the imaging sensor SR is recorded in a memory (e.g., a semiconductor memory, an optical disk) as a digital image signal after subjected to predetermined digital image processing, image compression processing and the like in accordance with a necessity, and is further transferred to other equipment via a cable or as it is converted into an infrared signal in some cases. The CCD may be replaced with a CMOS (Complementary Metal-oxide Semiconductor) sensor.

[0017] Figs. 1 through 10 are drawings which show lens arrangements of zoom lens systems disposed in imaging lens devices according to the first preferred embodiment through a tenth preferred embodiment in a condition that the zoom lens systems are in a minimum focal length state. In all preferred embodiments, the zoom lens system is a 3-component type zoom lens system which comprises a first unit Gr1 having a negative power, a second unit Gr2 having a positive power and a third unit Gr3 having a negative power in this order from the object side and changes gaps between the units for zooming. Further, in each embodiment, a parallel flat plate LPF which is outermost toward the image side belongs to a filter category including an optical low pass filter.

[0018] In the zoom lens system according to the first preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has an aspheric surface directed toward the image side and which is convex toward the object side and a positive meniscus lens element L2 which is convex toward the object side. The second unit Gr2 comprises an aperture stop ST, a cemented lens element DL1 (La), which comprises a negative meniscus lens element L3 (La1) which has an aspheric surface directed toward the object side and which convex toward the object side, a positive lens element L4 (La2) whose both surfaces are convex surfaces and a negative lens element

L5 (La3) whose both surfaces are concave surfaces, and a positive lens element L6 (Lb) whose both surfaces are convex surfaces. The third unit Gr3 comprises a positive meniscus lens element L7 which is convex toward the object side.

[0019] In the zoom lens system according to the second preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has an aspheric surface directed toward the image side and which is convex toward the object side and a positive meniscus lens element L2 which is convex toward the object side. The second unit Gr2 comprises an aperture stop ST, a cemented lens element DL1 (La), which comprises a negative meniscus lens element L3 (La1) which has an aspheric surface directed toward the object side and which is convex toward the object side, a positive lens element L4 (La2) whose both surfaces are convex surfaces and a negative lens element L5 (La3) whose both surfaces are concave surfaces, and a positive lens element L6 (Lb) which has an aspheric surface directed toward the image side and whose both surfaces are convex surfaces. The third unit Gr3 comprises a positive meniscus lens element L7 which is convex toward the object side.

[0020] In the zoom lens system according to the third preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has an aspheric surface directed toward the image side and which is convex toward the object side and a positive meniscus lens element L2 which is convex toward the object side. The second unit Gr2 comprises an aperture stop ST, a cemented lens element DL1 (La), which comprises a positive meniscus lens element L3 (La1) which has an aspheric surface directed toward the object side and which is convex toward the object side, a positive lens element L4 (La2) whose both surfaces are convex surfaces and a negative lens element L5 (La3) whose both surfaces are concave surfaces, and a positive lens element L6 (Lb) whose both surfaces are convex surfaces. The third unit Gr3 comprises a

positive meniscus lens element L7 which has an aspheric surface directed toward the object side and is convex toward the object side.

[0021] In the zoom lens system according to the fourth preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has an aspheric surface directed toward the image side and which is convex toward the object side and a positive meniscus lens element L2 which is convex toward the object side. The second unit Gr2 comprises an aperture stop ST, a cemented lens element DL1 (La), which comprises a negative meniscus lens element L3 (La1) which has an aspheric surface directed toward the object side and which is convex toward the object side, a positive meniscus lens element L4 (La2) which is convex toward the object side and a negative meniscus lens element L5 (La3) which is convex toward the object side, and a positive lens element L6 (Lb) whose both surfaces are convex surfaces. The third unit Gr3 comprises a positive meniscus lens element L7 which is convex toward the object side.

[0022] In the zoom lens system according to the fifth preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has aspheric surfaces on the both sides and which is convex toward the object side, a prism PR which bends an optical axis of an object ray by about 90 degrees (A reflection surface is not shown in the drawing.), and a cemented lens element DL1 which comprises a negative lens element L2 whose both surfaces are concave surfaces and a positive lens element L3 whose both surfaces are convex surfaces. The second unit Gr2 comprises an aperture stop ST, a cemented lens element DL2 (La), which comprises a positive lens element L4 (La1) which has an aspheric surface directed toward the object side and whose both surfaces are convex surfaces, a negative meniscus lens element L5 (La3) which is convex toward the image side and a negative lens element L6 (La3) whose both surfaces are concave surfaces, and a positive lens element L7 (Lb) whose both

surfaces are convex surfaces. The third unit Gr3 comprises a negative meniscus lens element L8 which is convex toward the image side and a positive lens element L9 which has aspheric surfaces on the both sides and whose both surfaces are convex surfaces.

[0023] In the zoom lens system according to the sixth preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has aspheric surfaces on the both sides and which is convex toward the object side, a prism PR which bends an optical axis of an object ray by about 90 degrees (A reflection surface is not shown in the drawing.), and a cemented lens element DL1 which comprises a negative lens element L2 whose both surfaces are concave surfaces and a positive lens element L3 whose both surfaces are convex surfaces. The second unit Gr2 comprises an aperture stop ST, a cemented lens element DL2 (La), which comprises a positive lens element L4 (La1) which has an aspheric surface directed toward the object side and which is convex toward the object side, a positive lens element L5 (La2) whose both surfaces are convex surfaces and a negative lens element L6 (La3) whose both surfaces are concave surfaces, and a positive lens element L7 (Lb) whose both surfaces are convex surfaces. The third unit Gr3 comprises a negative meniscus lens element L8 which is convex toward the image side and a positive lens element L9 which has aspheric surfaces on the both sides and whose both surfaces are convex surfaces.

[0024] In the zoom lens system according to the seventh preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has an aspheric surface directed toward the image side and which is convex toward the object side and a positive meniscus lens element L2 which is convex toward the object side. The second unit Gr2 comprises an aperture stop ST, a cemented lens element DL1 (La), which comprises a positive lens element L3 (La1) which has an aspheric surface directed

toward the object side and whose both surfaces are convex surfaces, a positive meniscus lens element L4 (La2) which is convex toward the image side and a negative lens element L5 (La3) whose both surfaces are concave surfaces, and a positive lens element L6 (Lb) whose both surfaces are convex surfaces. The third unit Gr3 comprises a positive meniscus lens element L7 which is convex toward the object side.

[0025] In the zoom lens system according to the eighth preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has an aspheric surface directed toward the image side and which is convex toward the object side and a positive meniscus lens element L2 which is convex toward the object side. The second unit Gr2 comprises an aperture stop ST and a cemented lens element DL1 (La) which comprises a positive lens element L3 (Lb) which has an aspheric surface directed toward the object side and whose both surfaces are convex surfaces, a positive meniscus lens element L4 (La1) whose both surfaces are convex surfaces, a positive meniscus lens element L5 (La2) which is convex toward the image side and a negative lens element L6 (La3) whose both surfaces are concave surfaces. The third unit Gr3 comprises a positive lens element L7 whose both surfaces are convex surfaces.

[0026] In the zoom lens system according to the ninth preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has an aspheric surface directed toward the image side and which is convex toward the object side and a positive meniscus lens element L2 which is convex toward the object side. The second unit Gr2 comprises an aperture stop ST and a cemented lens element DL1 (La) which comprises a positive lens element L3 (Lb) which has an aspheric surface directed toward the object side and whose both surfaces are convex surfaces, a negative lens element L4 (La2) which is convex toward the object side, a positive lens element L5 (La2) whose both surfaces are convex surfaces and a negative lens element L6 (La3)

whose both surfaces are concave surfaces. The third unit Gr3 comprises a positive lens element L7 whose both surfaces are convex surfaces.

[0027] In the tenth preferred embodiment, the first unit Gr1 comprises a negative meniscus lens element L1 which has an aspheric surface directed toward the image side and which is convex toward the object side and a positive meniscus lens element L2 which is convex toward the object side. The second unit Gr2 comprises an aperture stop ST and a cemented lens element DL1 (La) which comprises a positive lens element L3 (Lb) which has an aspheric surface directed toward the object side and whose both surfaces are convex surfaces, a positive meniscus meniscus lens element L4 (La1) which is convex toward the object side, a negative meniscus lens element L5 (La2) which is convex toward the object side and a negative meniscus lens element L6 (La3) which is convex toward the object side. The third unit Gr3 comprises a positive lens element L7 whose both surfaces are convex surfaces.

[0028] As described above, the zoom lens system according to each preferred embodiment is a zoom lens system which comprises the first unit Gr1 having a negative power, the second unit Gr2 having a positive power and the third unit Gr3 having a positive power and which changes gaps between the units for zooming, there is the aperture stop ST which restricts an on-axial luminous flux disposed between the first unit Gr1 and the second unit Gr2, and at least the second unit Gr2 comprises one cemented lens element La which is obtained by joining the three lens elements La1, La2 and La3 and one lens element Lb having a positive power. Of the three lens elements which form the cemented lens element La, the lens element La1 which is on the object side has a convex surface directed toward the object side, while the lens element La3 which is on the image surface side has a concave surface directed toward the image surface side.

[0029] Having the structures described above, the zoom lens systems according to the respective preferred embodiments further satisfy the following condition expressions:

$$-0.2 < (R_{21} - R_{24}) / (R_{21} + R_{24}) < 1.0 \quad (1)$$

$$0.6 < R_{21} / F_w < 10.0 \quad (2)$$

$$0.0 \leq h_2 / ha_4 < 1.0 \quad (3)$$

where

R_{21} : a paraxial radius of curvature of the object side-lens surface of the cemented lens element,

R_{24} : a paraxial radius of curvature of the image surface side-lens surface of the cemented lens element,

F_w : a focal length of the overall system at the wide-angle end,

ha_4 : a distance from an optical axis of an intersection of a principal ray which is at 0.8X of a maximum half-angle of view ω at the wide-angle end and the image surface side-lens surface of the cemented lens element,

h_2 : a distance from an optical axis of an intersection of a principal ray which is at 0.8X of a maximum half-angle of view ω at the wide-angle end and the outermost lens surface of the second unit toward the object side,

and where a principal ray is a ray which propagates on the center of the aperture stop.

[0030] Since these condition expressions are satisfied and owing to the structures described above, an aberration is corrected favorably particularly within the second unit Gr2, the optical system causes less change in aberration even during zooming, an eccentric sensitivity within the second unit Gr2 is suppressed, and adjustments during assembly are easy.

[0031] Of these condition expressions, the condition expression (1) is for

optimization of the shape of the cemented lens element La. When the cemented lens element La exceeds the upper limit value appearing in the condition expression (1), a spherical aberration, a coma and the like become excessively large in the cemented lens element La, it becomes difficult to correct an aberration and the thickness of the cemented lens element La along an optical axis direction increases, which is not desirable. On the contrary, when the cemented lens element La falls short of the lower limit value appearing in the condition expression (1), the Petzval's sum in the second unit Gr2 becomes large, which makes it difficult to correct a curvature of field. As for the condition expression (1), it is preferable that any one of the following relationships is satisfied for a further improvement of the effect described above:

$$0.0 < (R_{21} - R_{24}) / (R_{21} + R_{24}) \quad (1)'$$

$$(R_{21} - R_{24}) / (R_{21} + R_{24}) < 0.3 \quad (1)''$$

[0032] Meanwhile, the condition expression (2) is for optimization of the radius of curvature of the outermost lens surface of the cemented lens element La toward the object side. When the cemented lens element La falls short of the lower limit value appearing in the condition expression (2), an eccentric sensitivity of La becomes too high, which is not desirable. On the contrary, when the cemented lens element La exceeds the upper limit value appearing in the condition expression (2), the total length becomes long and it is not therefore possible to obtain a compact zoom lens system. As for the condition expression (2), it is preferable that any one of the following relationships is satisfied for a further improvement of the effect described above:

$$1.0 < R_{21} / F_w \quad (2)'$$

$$R_{21} / F_w < 3.0 \quad (2)''$$

[0033] The condition expression (3) is for restricting the height at which a principal ray travels within the second unit, and when the cemented lens goes outside the range

defined above, it becomes difficult to correct an astigmatism. As for the condition expression (3), it is preferable that the following relationship is satisfied for a further improvement of the effect described above:

$$0.0 \leq h_2 / h_{a4} < 0.5 \quad (3)'$$

[0034] It is further preferable to satisfy the following condition expressions described below, in addition to the condition expressions above.

[0035] It is desirable that the zoom lens system according to each preferred embodiment satisfies the following condition expression (4) below:

$$-0.7 < f_b / f_a < 1.2 \quad (4)$$

where

f_a : a focal length of the cemented lens element La, and

f_b : a focal length of the lens element Lb which has a positive power.

[0036] The condition expression (4) expresses an optimal range of a ratio of the focal length of the lens element Lb to the focal length of the cemented lens element La. When the lens elements fall short of the lower limit value appearing in the condition expression (4), a relative eccentric sensitivity of the cemented lens element La and the lens element Lb becomes high, which is not desirable. On the contrary, when the lens elements exceed the upper limit value, it becomes difficult to correct a spherical aberration, a coma, etc., the gap between the cemented lens element La and the lens element Lb increases, and a compact zoom lens system cannot be therefore obtained. As for the condition expression (4), it is preferable that any one of the following relationships is satisfied for a further improvement of the effect described above:

$$0.1 < f_b / f_a \quad (4)'$$

$$f_b / f_a < 0.5 \quad (4)''$$

[0037] As in the zoom lens system according to each preferred embodiment, the

lens element La3 preferably has a negative power and is characterized in satisfying the following condition expression:

$$23 < (Nd - 1) / (NF - NC) < 45 \quad (5)$$

where

Nd : a refractive index of the lens element La3 at the d-line (587.56 nm),

NF : a refractive index of the lens element La3 at the F-line (486.13 nm), and

NC : a refractive index of the lens element La3 at the C-line (656.28 nm).

[0038] The condition expression (5) is for optimization of the Abbe's number of the lens element La3 which is outermost to the image surface side among the three lens elements which form the cemented lens element La described earlier. When the lens goes beyond the upper limit value and the lower limit value appearing in the condition expression (5), a chromatic aberration becomes too large and it becomes difficult to correct a chromatic aberration.

[0039] In the zoom lens system according to each preferred embodiment, it is desirable that the outermost lens surface of the second unit Gr2 toward the object side is an aspheric surface. Such a structure makes it possible to favorably correct a spherical aberration, a coma and the like which develop at this lens surface, and therefore, is effective in suppressing a change in aberration due to an eccentric sensitivity, a core thickness error, etc. On the contrary, when an aspheric surface is provided at the outermost lens surface of the cemented lens element La toward the image side or one of the lens elements of the second unit Gr2 which is on the image side, it is possible to favorably correct an off-axis aberration.

[0040] Further, it is desirable that the first unit Gr1 has a doublet structure comprising a negative meniscus lens which has an aspheric surface and is convex toward the object side and a positive meniscus lens which is convex toward the object

side as in the zoom lens systems according to the first through the fourth and the seventh through the tenth preferred embodiments. Such a structure is simple and advantageously reduces the size. Alternatively, the first unit Gr1 may have a structure that two negative lens elements and one positive lens are used and at least one lens has an aspheric surface as in the zoom lens systems according to the fifth and the sixth preferred embodiments, in which case it is possible to move favorably correct an aberration. In addition, when the first unit Gr1 comprises two negative lens elements and one positive lens, any lens elements may be joined to each other.

[0041] Further, it is desirable that the aperture stop ST is disposed in front of the second unit Gr2 and moved as one unit together with the second unit Gr2 as in the zoom lens system according to each preferred embodiment. Such a structure is desirable in that it simplifies a mechanism of holding an aperture stop member. In terms of optical capabilities, too, this structure allows to favorably maintain a telecentric characteristic and align the imaging sensor to the location of a pupil.

[0042] As in the zoom lens system according to each preferred embodiment, it is desirable that the lens element Lb of the second unit Gr2 is a single lens whose both surfaces are convex surfaces. Such a structure permits to suppress an eccentric sensitivity without deteriorating an imaging capability. Further, since a single lens is used, this structure is preferable in an effort to reduce the size and lower the price.

[0043] It is desirable that the third unit Gr3 comprises one lens or two as in the zoom lens system according to each preferred embodiment, since this unit is close to the imaging surface and a sensitivity at an aberration-creating surface is relatively low. Such a structure is simple and realizes a compact zoom lens system. In addition, when the third unit Gr3 uses a plastic lens, a cost reduction is better attained. While a plastic lens generally has a problem that birefringence is intense and deteriorates an imaging

capability, use within the third unit Gr3 which is located relatively close to the image surface permits a plastic lens to exert only a minor influence.

[0044] In the zoom lens systems according to the fifth and the sixth preferred embodiments, the first unit comprises the prism PR which has a reflection surface so as to bend an optical axis of an object ray by about 90 degrees. Such a structure that a reflection surface bends an optical axis of an object ray by about 90 degrees, unlike a zoom lens of the collapsible mount type, allows to reduce the size of the imaging lens device in the thickness direction down to the size from the outermost lens toward the object side to the reflection surface both during use and nonuse, and therefore, is desirable as the apparent thickness of the imaging lens device is thin. In addition, owing to the structure that the reflection surface bends an optical axis of an object ray by about 90 degrees, it is possible to overlay optical paths of object rays with each other in the vicinity of the reflection surface, effectively use the space and further reduce the size of the imaging lens device.

[0045] While the reflection surface may either be (a) an internal reflection prism (as in the preferred embodiments), ((b) an internal reflection flat plate mirror or (c) a surface reflection mirror, use of (a) an internal reflection prism is most suitable. When an internal reflection prism is used, an object ray passes through a medium, and hence, an equivalent inter-surface gap at the time of passage through the prism is shorter than an actual gap in accordance with a refractive index of the medium. Use of an internal reflection prism as the reflection surface, therefore, realizes an optically equivalent structure even in a more compact space, which is desirable.

[0046] When the first unit comprises the prism PR which has a reflection surface so as to bend an optical axis of an object ray by about 90 degrees, it is desirable to fix the first unit relative to the imaging sensor. With the first unit fixed, a lens-barrel structure

which holds the respective lens elements is simplified and a thin imaging lens device whose total length does not change during zooming is accordingly obtained.

[0047] While each lens unit of each preferred embodiment comprises only refracting lens elements which deflect an incident ray by means of refraction (that is, lens elements in which deflection occurs at an interface between mediums which have different refractive indices from each other), this is not limiting. For instance, each lens unit may comprise diffracting lens elements which deflect an incident ray by means of diffraction, refraction/diffraction hybrid lens elements which deflect an incident ray by means of a combination of diffraction and refraction, refractive index distribution lens elements which deflect an incident ray by means of a refractive index distribution within a medium, or the like.

[0048] A structure and the like of a zoom lens system installed in an imaging lens device to which the present invention is applied will now be described more specifically with reference to construction data, aberration diagrams, etc. A first through a tenth examples described below correspond respectively to the first preferred embodiment through the tenth preferred embodiment described above, and lens structure diagrams (Figs. 1 through 10) representing the first through the tenth preferred embodiments respectively show lens structures according to the first through the tenth examples.

[0049] With respect to construction data regarding the respective examples, r_i ($i = 1, 2, 3, \dots$) denotes a radius of curvature (mm) of an i -th surface from the object side, d_i ($i = 1, 2, 3, \dots$) denotes an i -th on-axial inter-surface gap (mm) from the object side, and N_i ($i = 1, 2, 3, \dots$) and v_i ($i = 1, 2, 3, \dots$) denote a refractive index (Nd) and the Abbe's number (vd) of an i -th optical element from the object side to the d-line. Further, among the construction data, an on-axial inter-surface gap which changes during zooming represents a value of variable gap which changes between a minimum focal

length state (wide-angle end), an intermediate focal length state (middle) and a maximum focal length state (telephoto end). A focal length (f , mm) and the F-number (FNO) of the entire system in each one of the focal length states (wide-angle end), (middle) and (telephoto end) are shown together with other data.

[0050] When the symbol * is added to r_i which is the symbol for the radius of curvature, this surface is an aspheric surface whose shape is defined by the following formula (AS). Aspheric surface data according to the respective examples are shown together with other data.

$$x = \frac{C_0 y^2}{1 + \sqrt{1 - \varepsilon C_0^2 y^2}} + \sum A_i y^i \quad (AS)$$

where,

x represents the shape (mm) of the aspherical surface (i.e., the displacement along the optical axis at the height y in a direction perpendicular to the optical axis of the aspherical surface),

C_0 represents the curvature (mm^{-1}) of the reference aspherical surface of the aspherical surface,

y represents the height in a direction perpendicular to the optical axis,

ε represents the quadric surface parameter, and

A_i represents the aspherical coefficient of order i .

<Example 1>

f = 3.7 · 6.4 · 11.0
Fno.= 2.80 · 3.48 · 4.83

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1 = 16.705	d1 = 0.800	N1 = 1.77377	v1 = 47.17
r2* = 3.391	d2 = 1.322		
r3 = 5.368	d3 = 1.754	N2 = 1.84666	v2 = 23.78
r4 = 8.849	d4 = 11.278 · 4.711 · 1.500		
r5 = INF (ST)	d5 = 0.100		
r6* = 25.241	d5 = 0.800	N3 = 1.48749	v3 = 70.44
r7 = 3.517	d6 = 1.317	N4 = 1.80610	v4 = 40.72
r8 = -108.976	d7 = 0.902	N5 = 1.84666	v5 = 23.78
r9 = 5.054	d8 = 0.380 · 7.938 · 15.835		
r10 = 7.436	d10 = 1.683	N6 = 1.48749	v6 = 70.44
r11 = -4.738	d11 = 3.380 · 7.938 · 15.835		
r12 = 10.056	d12 = 1.148	N7 = 1.61800	v7 = 63.39
r13 = 59.062	d13 = 3.236 · 2.639 · 0.562		
r14 = INF	d14 = 1.700	N8 = 1.51680	v8 = 64.20
r15 = INF			

[Aspherical Coefficient]

r2*
 ϵ = 0.19470
A4 = 0.11620E-02
A6 = 0.95462E-05
A8 = 0.20237E-05
A10 = -0.2884E-07

r6*
 ϵ = -203.29
A4 = -0.83358E-03
A6 = -0.31617E-03
A8 = -0.12511E-04

A10= 0.15435E-04
A12=-0.35460E-05

<Example 2>

f = 3.7 · 6.4 · 11.0
Fno.= 2.80 · 3.44 · 4.72

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	[Abbe Number (vd)]
r1 = 18.622	d1 = 0.800	N1 = 1.80420	v1 = 46.50
r2* = 3.415	d2 = 1.446		
r3 = 5.592	d3 = 1.65193	N2 = 1.84666	v2 = 23.78
r4 = 9.598	d4 = 11.539 · 4.782 · 1.500		
r5 = INF(ST)	d5 = 0.100		
r6* = 6.033	d6 = 1.344	N3 = 1.80518	v3 = 25.46
r7 = 3.937	d7 = 1.768	N4 = 1.80420	v4 = 46.50
r8 = -4.807	d8 = 0.800	N5 = 1.59270	v5 = 35.45
r9 = 4.664	d9 = 0.986		
r10 = 11.144	d10 = 1.017	N6 = 1.58913	v6 = 61.25
r11* = -33.891	d11 = 3.643 · 6.446 · 12.546		
r12 = 8.711	d12 = 1.248	N7 = 1.61800	v7 = 63.39
r13 = 89.713	d13 = 0.75770		
r14 = INF	d14 = 1.70000	N8 = 1.51680	v8 = 64.20
r15 = INF			

[Aspherical Coefficient]

r2
 ϵ = 0.16362
A4 = 0.10888E-02
A6 = 0.22967E-04
A8 = 0.77583E-06
A10 = -0.14352E-07

r6
 ϵ = 1.1149
A4 = -0.93987E-03
A6 = 0.23171E-04
A8 = -0.19816E-04

A10= 0.23207E-05

r11
e=-26.231
A4 = 0.37264E-03
A6 = 0.70165E-04
A8 =-0.20813E-05
A10=-0.18058E-05
A12= 0.19225E-06

<Example 3>

f = 3.7 · 6.4 · 11.0
Fno.= 2.80 · 3.46 · 4.71

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1 = 26.372	d1 = 0.800	N1 = 1.69350	v1 = 53.20
r2* = 3.261	d2 = 1.306		
r3 = 5.374	d3 = 1.643	N3 = 1.84666	v2 = 23.78
r4 = 8.587	d4 = 11.113 · 4.730 · 1.500		
r5 = INF(ST)	d5 = 0.100		
r6* = 6.440	d6 = 2.700	N4 = 1.58313	v3 = 59.46
r7 = 21.791	d7 = 0.992	N5 = 1.80420	v4 = 46.50
r8 = -17.258	d8 = 0.800	N6 = 1.84666	v5 = 23.78
r9 = 9.052	d9 = 0.461		
r10 = 32.852	d10 = 1.185	N7 = 1.80420	v6 = 46.50
r11 = -8.295	d11 = 3.264 · 7.269 · 14.682		
r12* = 8.698	d12 = 1.151	N8 = 1.52510	v7 = 56.38
r13 = 40.251	d13 = 2.395 · 2.146 · 0.589		
r14 = INF	d14 = 1.700	N9 = 1.51680	v8 = 64.20
r15 = INF			

[Aspherical Coefficient]

r2
 ϵ = 0.15350
A4 = 0.10709E·02
A6 = 0.15594E·05
A8 = 0.40992E·05
A10 = -0.14072E·06

r6
 ϵ = 0.99639
A4 = -0.10102E·02
A6 = 0.13282E·03
A8 = -0.61751E·04

A10= 0.89979E-05

r12

ϵ = 0.18574

A4 =-0.22753E-03

A6 = 0.22152E-04

A8 =-0.20494E-05

A10=-0.24795E-06

A12 =0.31566E-07

<Example 4>

$$f = 4.3 \cdot 7.4 \cdot 12.7$$
$$Fno.= 2.80 \cdot 3.50 \cdot 4.82$$

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1 = 20.370	d1 = 0.800	N1 = 1.80420	v1 = 46.50
r2* = 3.853	d2 = 1.381		
r3 = 6.112	d3 = 1.676	N2 = 1.84666	v2 = 23.78
r4 = 11.173	d4 = 12.341 · 5.133 · 1.500		
r5 = INF(ST)	d5 = 0.100		
r6* = 3.144	d6 = 0.800	N3 = 1.81474	v3 = 37.03
r7 = 2.393	d7 = 1.341	N4 = 1.58913	v4 = 61.25
r8 = 5.699	d8 = 0.800	N5 = 1.84666	v5 = 23.78
r9 = 2.911	d9 = 1.194		
r10 = 6.125	d10 = 1.356	N6 = 1.61800	v6 = 63.39
r11 = -14.481	d11 = 3.387 · 7.171 · 14.068		
r12 = 8.013	d12 = 1.222	N7 = 1.61800	v7 = 63.39
r13 = 31.092	d13 = 1.684 · 1.633 · 0.617		
r14 = INF	d14 = 1.700	N8 = 1.61800	v8 = 64.20
r15 = INF			

[Aspherical Coefficient]

$$r2$$
$$\epsilon = 0.082016$$
$$A4 = 0.89031E\cdot 03$$
$$A6 = 0.85045E\cdot 05$$
$$A8 = 0.52996E\cdot 06$$
$$A10 = -0.28440E\cdot 08$$

$$r6$$
$$\epsilon = 0.98430$$
$$A4 = -0.11022E\cdot 02$$
$$A6 = -0.43928E\cdot 04$$
$$A8 = -0.14368E\cdot 04$$

A10= 0.19844E-06

<Example 5>

$$f = 4.8 \cdot 8.3 \cdot 14.4$$
$$Fno. = 2.40 \cdot 3.48 \cdot 4.88$$

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1*=18.302	d1 = 0.700	N1 = 1.77377	v1 = 47.17
r2*= 5.330	d2 = 2.312		
r3 = INF	d3 = 7.300	N2 = 1.84666	v2 = 23.78
r4 = INF	d4 = 1.058		
r5 = -10.423	d5 = 0.700	N3 = 1.67003	v3 = 47.20
r6 = 12.817	d6 = 2.059	N4 = 1.83400	v4 = 37.34
r7 = -14.332	d7 = 14.836 · 7.674 · 0.600		
r8 = INF(ST)	d8 = 0.100		
r9*= 6.792	d9 = 1.764	N5 = 1.74330	v5 = 49.33
r10=-63.330	d10= 2.457	N6 = 1.56883	v6 = 56.04
r11=-138.507	d11= 0.700	N7 = 1.75520	v7 = 27.53
r12= 5.578	d12= 0.831		
r13=17.227	d13= 1.267	N8 = 1.71300	v8 = 53.94
r14=-23.244	d14= 0.726 · 11.724 · 21.069		
r15=-11.747	d15= 0.700	N9 = 1.67270	v9 = 32.17
r16=-169.983	d16= 0.200		
r17*= 9.384	d17= 2.179	N10= 1.52200	v10= 52.20
r18*= -13.516	d18= 6.703 · 2.867 · 0.595		
r19= INF	d19= 1.400	N11= 1.54426	v11= 69.60
r20= INF	d20= 0.500		
r21= INF	d21= 0.500	N12= 1.51680	v12= 64.20
r22= INF			

[Aspherical Coefficient]

r1

$\epsilon = 1.00000$

A4 = 0.27232E-04

A6 = 0.39408E-05

A8 = -0.14135E-06

A10 = 0.21831E-08

r2

$\epsilon = 1.00000$

A4 = -0.34005E-03

A6 = -0.54077E-05

A8 = 0.11468E-06

A10 = -0.26766E-07

r9

$\epsilon = 1.00000$

A4 = -0.18052E-03

A6 = -0.13514E-05

A8 = -0.15509E-06

A10 = 0.35394E-08

r17

$\epsilon = 1.00000$

A4 = 0.35361E-03

A6 = 0.18176E-04

A8 = 0.13001E-05

A10 = 0.99636E-07

r18

$\epsilon = 1.00000$

A4 = 0.70533E-03

A6 = 0.39821E-04

A8 = -0.19361E-05

A10 = 0.33293E-06

<Example 6>

$$f = 4.8 \cdot 7.8 \cdot 12.8$$
$$Fno.= 2.58 \cdot 3.57 \cdot 4.80$$

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1*=22.792	d1 = 1.000	N1 = 1.80432	v1 = 40.90
r2*= 6.229	d2 = 2.500		
r3 = INF	d3 = 7.200	N2 = 1.84666	v2 = 23.82
r4 = INF	d4 = 0.831		
r5 =-24.708	d5 = 0.500	N3 = 1.51680	v3 = 64.20
r6 = 8.329	d6 = 2.145	N4 = 1.62004	v4 = 36.29
r7 =-32.788	d7 = 15.275 - 8.982 - 2.800		
r8 = INF	d8 = 0.000		
r9*= 6.608	d9 = 2.471	N5 = 1.68893	v5 = 31.16
r10= 5.889	d10= 1.489	N6 = 1.77250	v6 = 49.62
r11=-56.295	d11= 0.500	N7 = 1.74077	v7 = 27.76
r12= 5.472	d12= 0.711		
r13= 16.423	d13= 1.138	N8 = 1.74330	v8 = 49.22
r14=-28.916	d14 = 1.170 - 10.323 - 18.245		
r15=-8.438	d15 = 0.800	N9 = 1.67270	v9 = 32.17
r16=-27.478	d16 = 0.100		
r17*=14.047	d17 = 1.910	N10= 1.52200	v10= 52.20
r18*=-8.669	d18= 6.860 - 4.000 - 2.259		
r19= INF	d19= 1.400	N11= 1.54426	v11= 69.60
r20= INF	d20= 0.500		
r21= INF	d21= 0.500	N12= 1.51680	v12= 64.20
r22= INF			

[Aspherical Coefficient]

r1
 $\epsilon = 5.4920$

r2
 $\epsilon = 1.0396$
 $A_4 = -0.15950E-03$
 $A_6 = -0.48677E-05$
 $A_8 = 0.11077E-06$
 $A_{10} = -0.71574E-08$

r9
 $\epsilon = 1.0745$
 $A_4 = -0.21338E-03$
 $A_6 = -0.27376E-05$
 $A_8 = -0.12249E-06$

r17
 $\epsilon = -12.880$
 $A_4 = 0.62509E-03$
 $A_6 = -0.46408E-04$
 $A_8 = 0.39484E-05$
 $A_{10} = -0.17953E-06$

r18
 $\epsilon = -0.99348$
 $A_4 = -0.13615E-05$
 $A_6 = -0.20891E-04$
 $A_8 = 0.15372E-05$
 $A_{10} = 0.49048E-08$
 $A_{12} = -0.53253E-08$

<Example 7>

f = 3.7 · 6.4 · 11.1
Fno.= 2.80 · 3.46 · 4.75

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1 = 19.994	d1 = 0.800	N1 = 1.80420	v1 = 46.50
r2* = 3.472	d2 = 1.546		
r3 = 5.850	d3 = 1.626	N2 = 1.84666	v2 = 23.78
r4 = 10.302	d4 = 11.856 · 5.036 · 1.500		
r5 = INF(ST)	d5 = 0.100		
r6* = 5.145	d6 = 1.264	N3 = 1.80420	v3 = 46.50
r7 = -10.464	d7 = 1.169	N4 = 1.48749	v4 = 70.44
r8 = -7.576	d8 = 0.800	N5 = 1.75520	v5 = 27.53
r9 = 4.564	d9 = 0.541		
r10 = 18.200	d10 = 1.063	N6 = 1.80420	v6 = 46.50
r11 = -10.526	d11 = 4.396 · 7.331 · 13.340		
r12 = 8.998	d12 = 1.244	N7 = 1.61800	v7 = 63.39
r13 = 129.377	d13 = 0.695 · 0.958 · 0.528		
r14 = INF	d14 = 1.700	N8 = 1.51680	v8 = 64.20
r15 = INF			

[Aspherical Coefficient]

r2
 ϵ = 0.25203
A4 = 0.70604E-03
A6 = 0.12790E-04
A8 = 0.74823E-06
A10 = -0.26178E-07

r6
 ϵ = 1.1462
A4 = -0.80387E-03
A6 = 0.63344E-05
A8 = -0.11753E-04

A10= 0.15469E-05

<Example 8>

f = 3.7 · 6.4 · 11.1
Fno.= 2.80 · 3.26 · 4.52

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1 = 15.437	d1 = 0.600	N1 = 1.77377	v1 = 47.17
r2* = 4.065	d2 = 2.427		
r3 = 6.638	d3 = 1.700	N2 = 1.84666	v2 = 23.78
r4 = 9.175	d4 = 14.094 · 4.624 · 0.758		
r5 = INF	d5 = 0.641		
r6* = 5.996	d6 = 1.600	N3 = 1.58913	v3 = 61.25
r7 = 7.178	d7 = 0.100		
r8 = 15.198	d8 = 1.405	N4 = 1.65160	v4 = 58.40
r9 = 3.484	d9 = 0.801	N5 = 1.80420	v5 = 46.50
r10 = -3.020	d10 = 0.600	N6 = 1.59551	v6 = 39.22
r11 = 3.194	d11 = 3.532 · 4.546 · 9.953		
r12* = 9.016	d12 = 1.500	N7 = 1.48749	v7 = 70.44
r13 = -16.883	d13 = 0.600 · 1.854 · 1.737		
r14 = INF	d14 = 1.700	N8 = 1.51680	v8 = 64.20
r15 = INF			

[Aspherical Coefficient]

r2
 ϵ = 0.047344
A4 = 0.87594E-03
A6 = 0.42505E-04
A8 = -0.19104E-05
A10 = 0.10896E-06

r6
 ϵ = 1.29260
A4 = -0.26982E-02
A6 = -0.11629E-03
A8 = -0.891545E-05

A10= 0.94521E-05
A12=-0.17799E-05

r12
 ε = -4.5109
A4 = 0.22605E-03
A6 = 0.13383E-03
A8 =-0.25198E-04
A10= 0.24106E-05
A12=-0.91614E-07

<Example 9>

$$f = 3.7 \cdot 6.4 \cdot 11.1$$
$$Fno.= 2.80 \cdot 3.32 \cdot 4.64$$

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1 = 21.845	d1 = 1.000	N1 = 1.77377	v1 = 47.17
r2* = 4.532	d2 = 2.285		
r3 = 7.397	d3 = 1.602	N2 = 1.84666	v2 = 23.78
r4 = 11.705	d4 = 14.749 - 4.896 · 0.714		
r5 = INF(ST)	d5 = 0.100		
r6* = 8.070	d6 = 1.716	N3 = 1.58913	v3 = 61.25
r7 = -6.828	d7 = 0.100		
r8 = 33.916	d8 = 0.600	N4 = 1.84666	v4 = 23.78
r9 = 10.422	d9 = 1.407	N5 = 1.80420	v5 = 46.50
r10 = -3.231	d10 = 1.717	N6 = 1.59551	v6 = 39.22
r11 = 3.154	d11 = 2.521 - 3.664 · 8.419		
r12* = 7.784	d12 = 1.200	N7 = 1.48749	v7 = 70.44
r13 = -32.962	d13 = 0.603 - 1.372 · 0.600		
r14 = INF	d14 = 1.700	N8 = 1.51680	v8 = 64.20
r15 = INF			

[Aspherical Coefficient]

$$r2$$
$$\epsilon = -0.057547$$
$$A4 = 0.73212E-03$$
$$A6 = 0.40379E-04$$
$$A8 = -0.30424E-05$$
$$A10 = 0.15307E-06$$
$$A12 = -0.27398E-08$$

$$r6$$
$$\epsilon = -2.3793$$
$$A4 = -0.26006E-02$$
$$A6 = -0.13413E-03$$

A8 = -0.78171E-05
A10 = 0.76194E-05
A12 = -0.18804E-05

r12
 ϵ = -2.9040
A4 = 0.67481E-03
A6 = 0.12901E-03
A8 = -0.19512E-04
A10 = 0.18944E-05
A12 = -0.74522E-07

<Example 10>

$f = 3.7 \cdot 6.4 \cdot 11.1$
 $Fno. = 2.80 \cdot 3.33 \cdot 4.62$

[Radius of Curvature]	[Axial Distance]	[Refractive Index(nd)]	
		[Abbe Number (vd)]	
r1 = 24.410	d1 = 0.600	N1 = 1.77377	v1 = 47.17
r2* = 4.632	d2 = 2.760		
r3 = 8.453	d3 = 1.180	N2 = 1.84666	v2 = 23.78
r4 = 13.342	d4 = 14.689 - 4.950 - 0.714		
r5 = INF(ST)	d5 = 1.000		
r6* = 7.302	d6 = 1.500	N3 = 1.58913	v3 = 61.25
r7 = -11.987	d7 = 0.100		
r8 = 3.463	d8 = 1.162	N4 = 1.48749	v4 = 70.44
r9 = 7.545	d9 = 0.600	N5 = 1.62588	v5 = 35.74
r10 = 6.356	d10 = 0.600	N6 = 1.84666	v6 = 23.78
r11 = 2.584	d11 = 3.271 - 4.536 - 9.744		
r12* = 7.280	d12 = 1.538	N7 = 1.48749	v7 = 70.44
r13 = -27.930	d13 = 0.600		
r14 = INF	d14 = 1.700	N8 = 1.51680	v8 = 64.20
r15 = INF			

[Aspherical Coefficient]

r2
 $\epsilon = 0.042158$
 $A4 = 0.45640E-03$
 $A6 = 0.37721E-04$
 $A8 = -0.27034E-05$
 $A10 = 0.12077E-06$
 $A12 = -0.20555E-08$

r6
 $\epsilon = 3.9934$
 $A4 = -0.17251E-02$
 $A6 = -0.52140E-04$

A8 = -0.55250E-05
A10 = 0.81274E-06
A12 = -0.65613E-07

r12
 ϵ = 0.20393
A4 = -0.18824E-03
A6 = 0.15999E-04
A8 = 0.10173E-04
A10 = -0.13747E-05
A12 = 0.55848E-07

[0051] Figs. 11 through 20 are aberration diagrams of the first through the tenth examples, each showing aberrations when the zoom lens system according to each example is an infinite focus state. Shown in Figs. 11 through 20 are aberrations in the minimum focal length state, the intermediate focal length state, the maximum focal length state from the top [Shown from the left hand side are spherical aberrations or the like, astigmatisms and distortion aberrations, and Y' (mm) denotes a maximum image height (which corresponds to a distance from the optical axis) on the imaging sensor.]. In the spherical aberration diagrams, the solid line (d) represents spherical aberrations to the d-line, the dashed line (g) represents spherical aberrations to the g-line, and the broken line (SC) represents the level of dissatisfaction of the sine condition. In the astigmatism diagrams, the broken line (DM) represents astigmatisms at a meriodional surface and the solid line (DS) represents astigmatisms at a sagital surface. In the distortion aberration diagrams, the solid line represents a distortion % to the d-line.

[0052] The table below shows values of conditional expressions (1) through (5) and values of a maximum half-angle of view ω in the respective examples.

Table

	Condition (1)	Condition (2)	Condition (3)	Condition (4)	Condition (5)	ω
Example 1	0.6663	6.8218	0.0568	-0.2174	23.78	34.15
Example 2	0.1280	1.6306	0.0447	1.1474	35.45	34.12
Example 3	-0.1686	1.7405	0.0368	0.2263	23.78	33.92
Example 4	0.0385	0.7311	0.0556	0.1486	23.78	30.06
Example 5	0.0981	1.4149	0.0330	0.2847	27.52	32.89
Example 6	0.0941	1.3768	0.0000	0.2811	27.75	32.00
Example 7	0.0598	1.3905	0.0503	0.3811	27.52	34.08
Example 8	0.6526	4.1067	0.2227	-0.6249	39.23	33.61
Example 9	0.8298	9.1665	0.0336	-0.5455	39.23	34.02
Example 10	0.1454	0.9360	0.3743	-0.5301	23.78	33.98

[0053] As described above, the zoom lens system according to each preferred embodiment allows to obtain an imaging lens device comprising a zoom lens system which has a low eccentric sensitivity but is compact and has an excellent optical capability.

[0054] Although the present invention has been fully described by way of example with reference to the accompanying drawings, it is to be understood that various changes and modifications will be apparent to those skilled in the art. Therefore, unless otherwise such changes and modification depart from the scope of the present invention, they should be construed as being included therein.